

Mitigating Non-linear DAC Glitches Using Dither in Closed-loop Nano-positioning Applications

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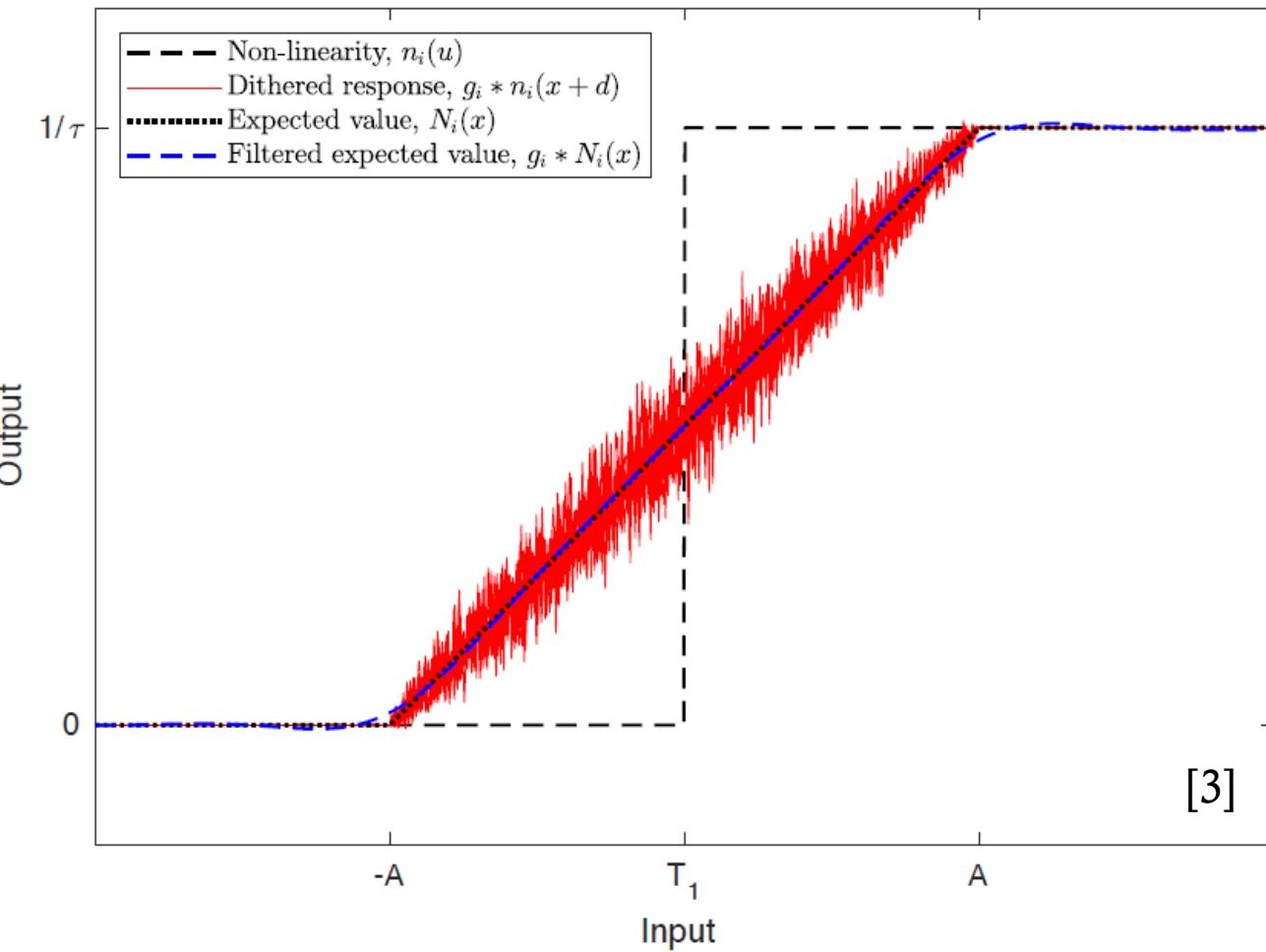
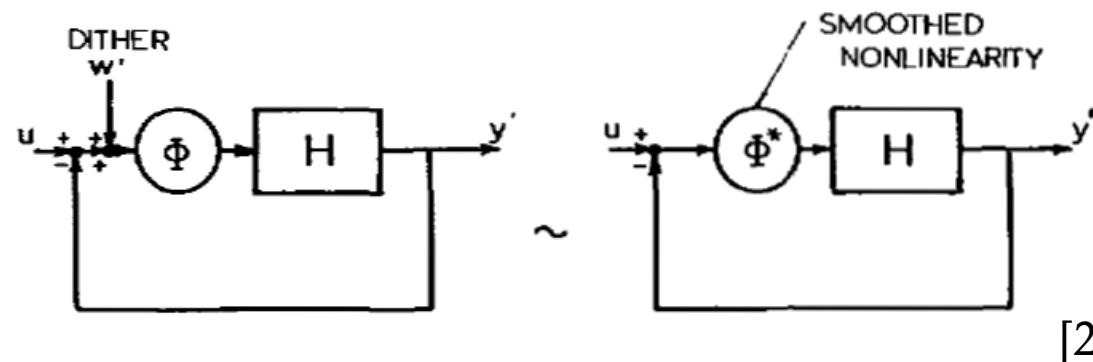
Main supervisor: Arnfinn A. Eielsen (UiS)

Co-supervisor: John-Josef Leth (AAU)



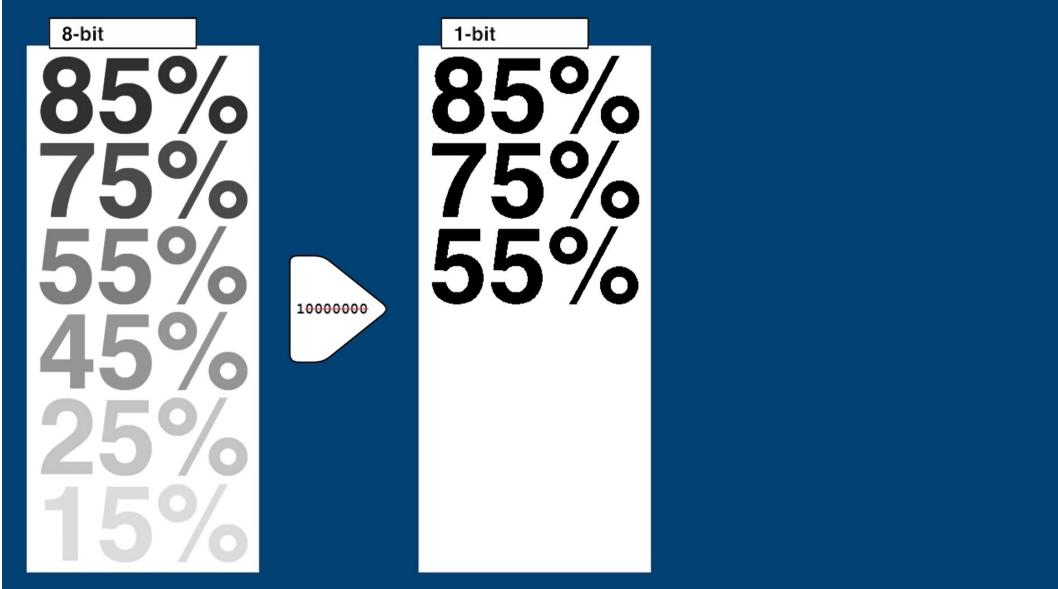
WHAT IS DITHERING?

- Dithering: is a process by which a form of noise is intentionally applied to a signal in order to randomize the quantization error (e.g. due to intended resolution reduction) [1].

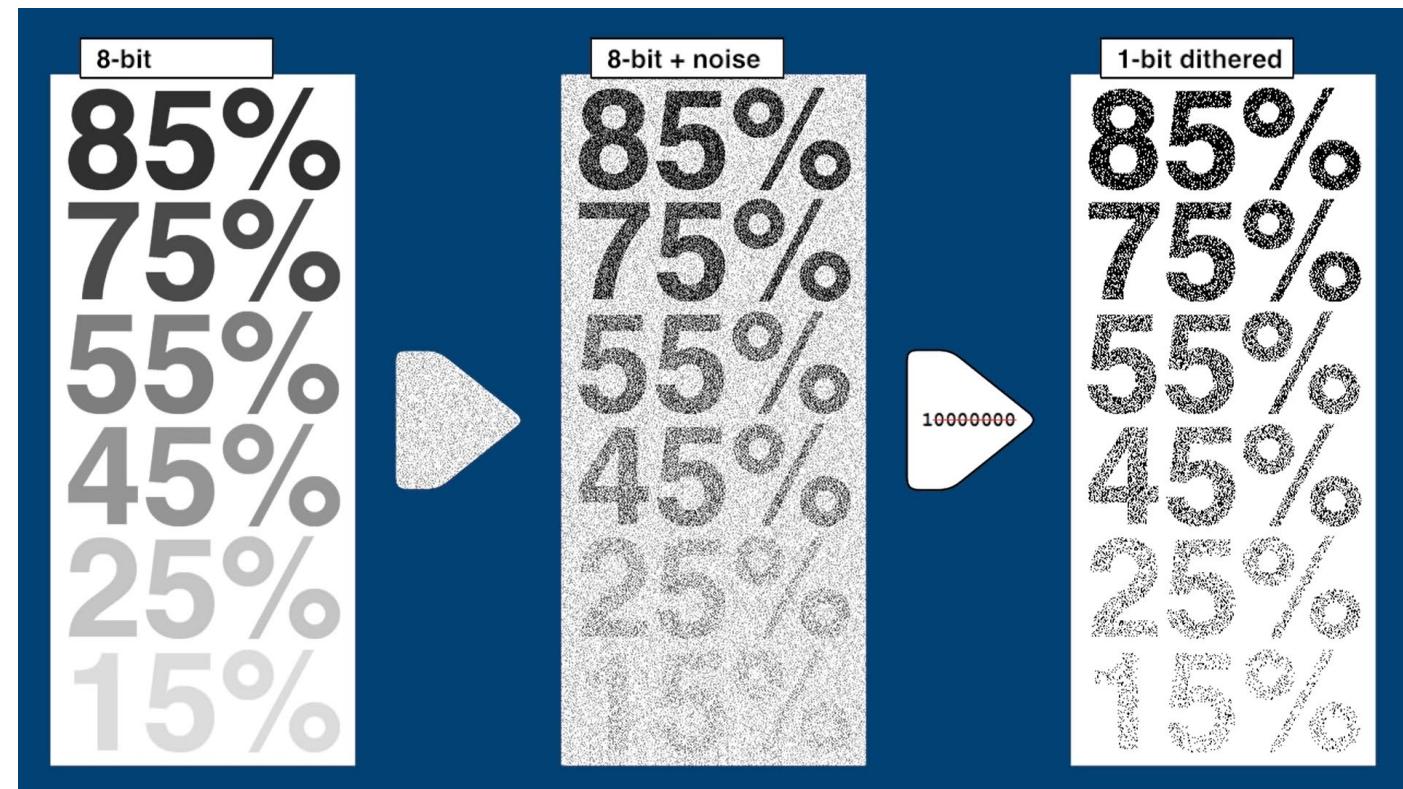


DITHERING EXAMPLE

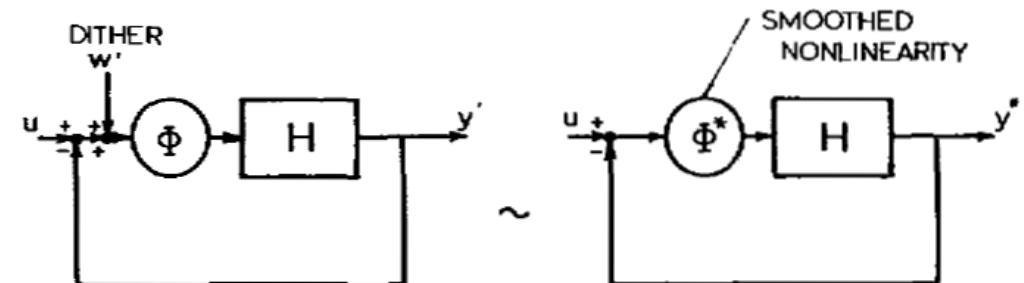
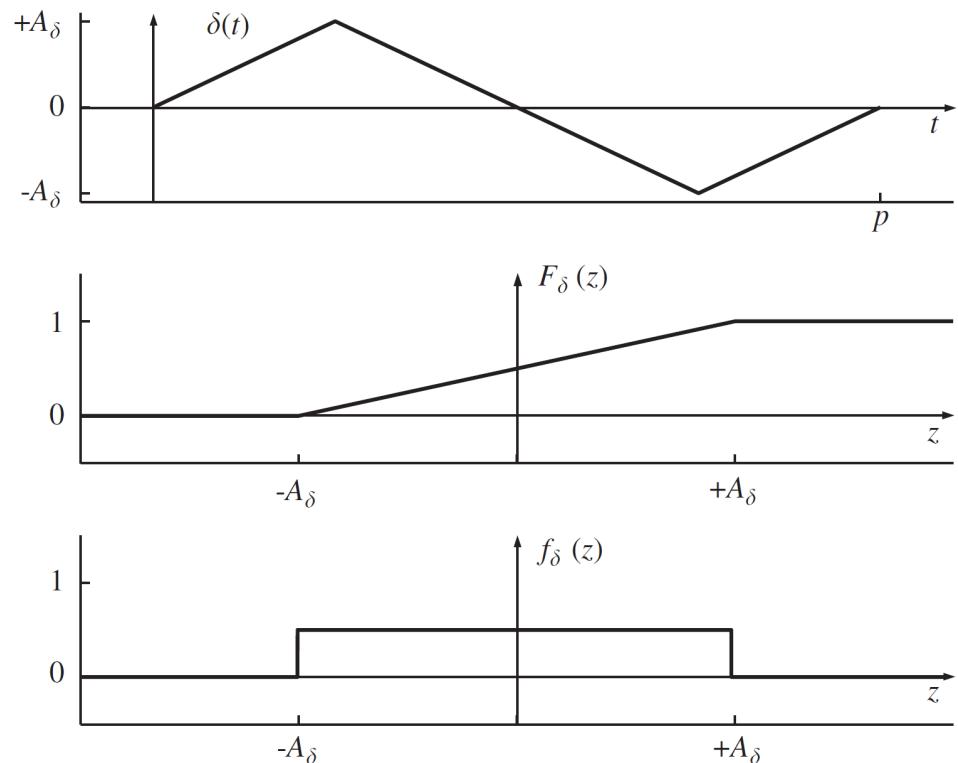
Ideal Quantization



Dithered system

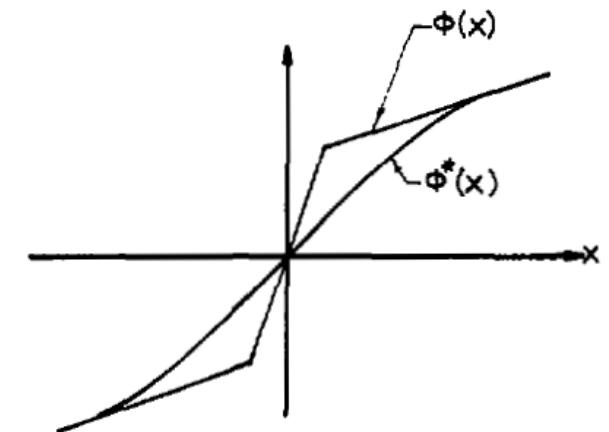


DITHER CHARACTERISTICS



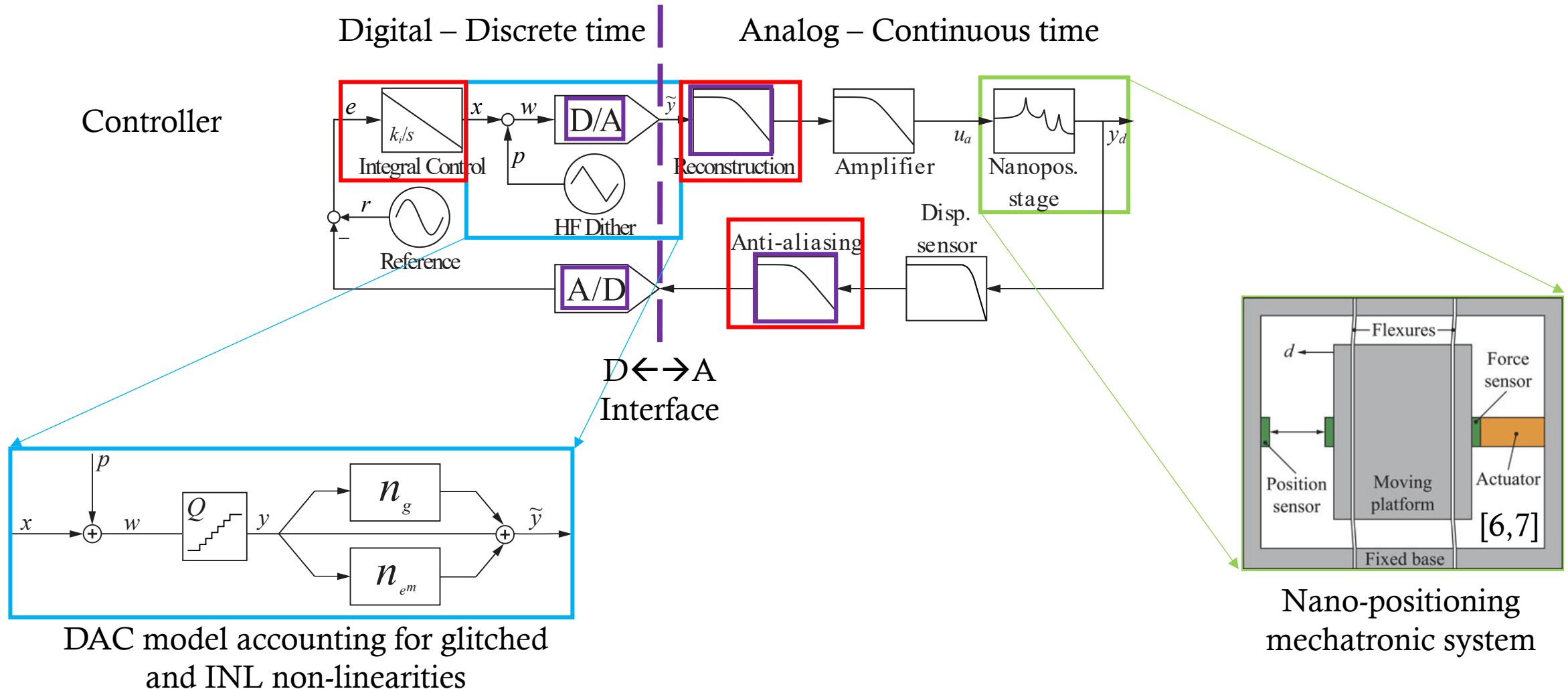
[2]

$$\begin{aligned}
 N(z) &\stackrel{\Delta}{=} \int_{\mathbb{R}} n(z + \xi) dF_{\delta}(\xi) \\
 &= \frac{1}{p} \int_{[0, p)} n(z + \delta(s)) ds \\
 &= \int_{\mathbb{R}} n(z + \xi) f_{\delta}(\xi) d\xi
 \end{aligned}$$



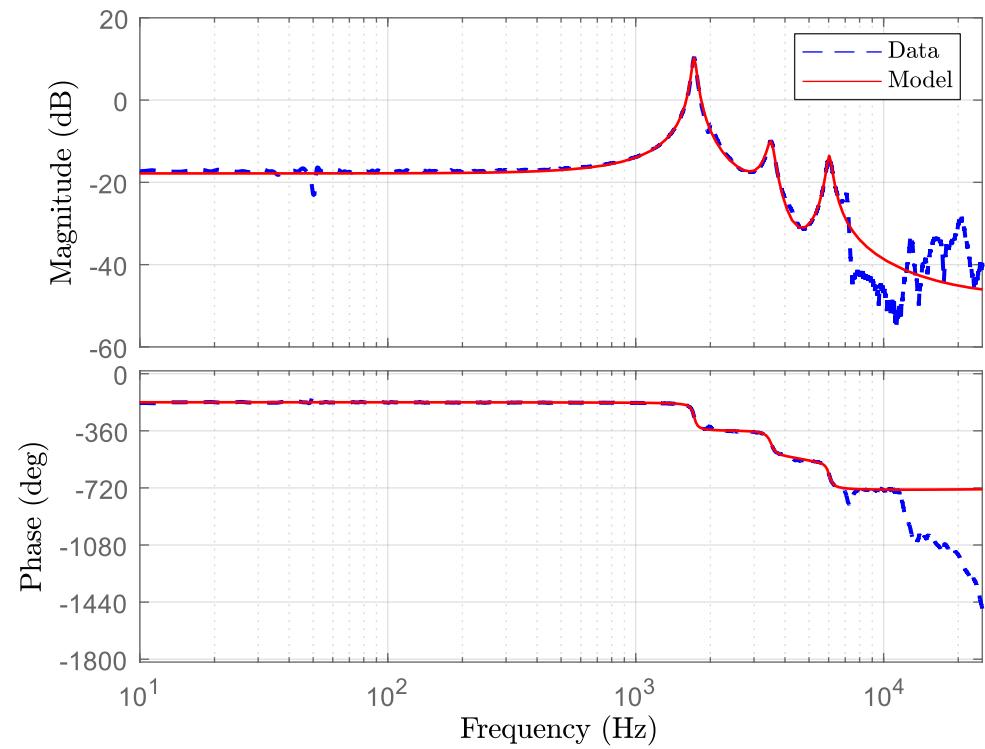
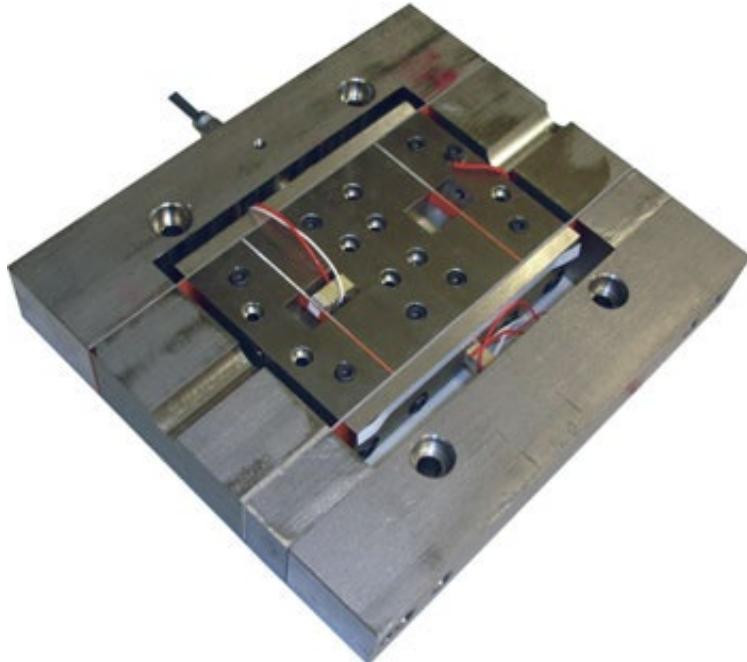
CLOSED-LOOP NANO-POSITIONING SYSTEM

[5]

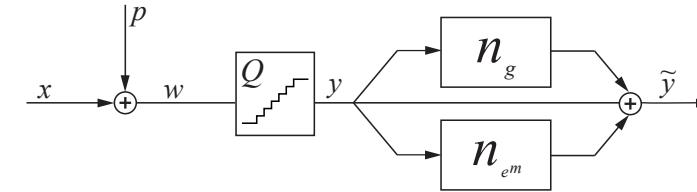


NANO-POSITIONING STAGE MODEL

- Response fitted to an Ultra high precision nano-positioning stage mechatronic system [6,7]

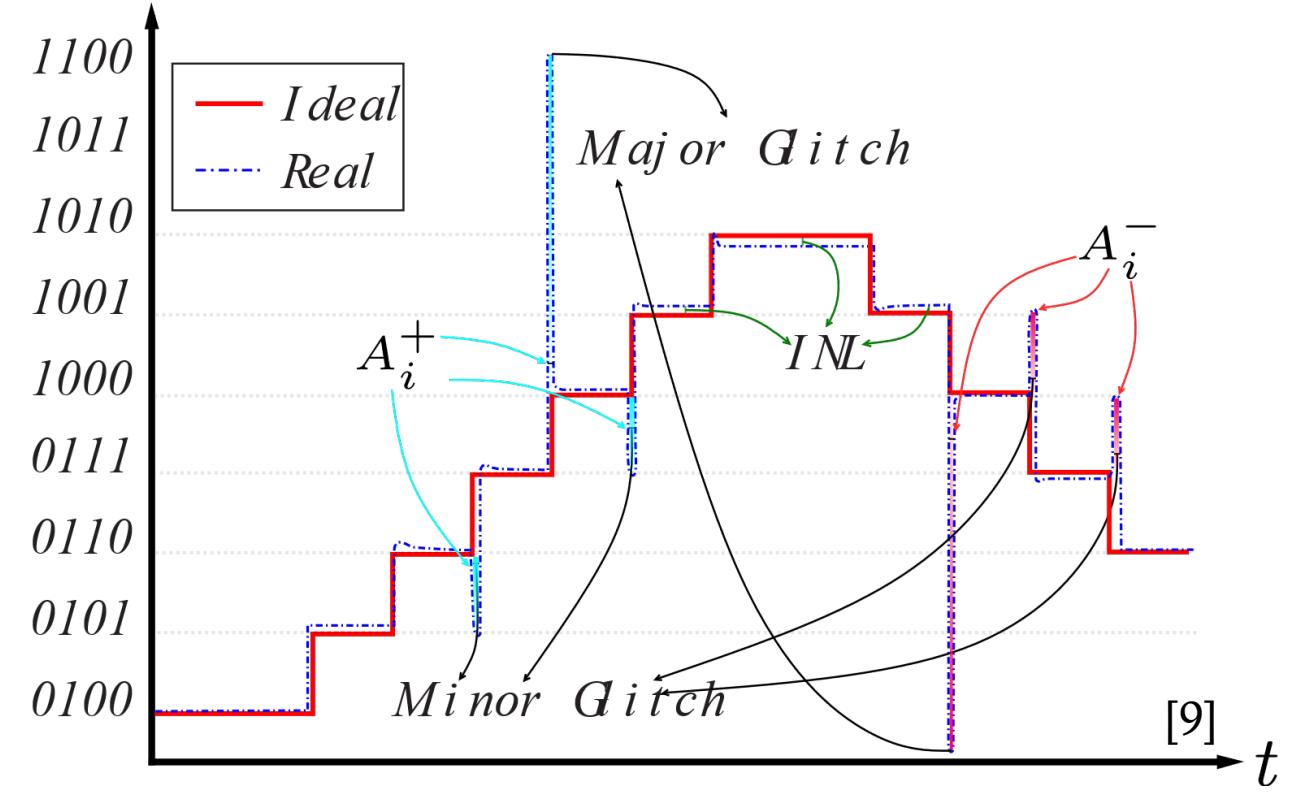


NON-LINEAR DAC MODEL



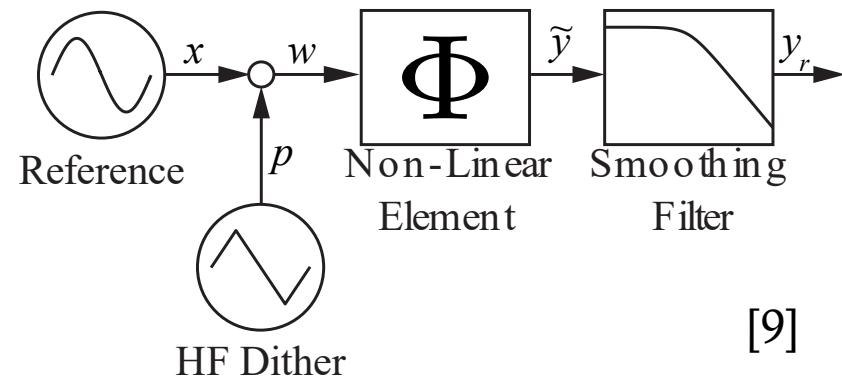
DAC model accounting for glitched and INL non-linearities for a 16-bit Texas Instruments DAC8544.

$$\left. \begin{array}{l} \text{Ideal Quantization} \\ \quad Q(w) = \delta T(w) = \delta \left\lfloor \frac{w}{\delta} + \frac{1}{2} \right\rfloor \\ \quad \delta = \frac{\Delta}{2^B - 1} \\ \\ n_{em} = \delta \text{INL}(w) \\ \text{INL}(w) \triangleq \frac{\tilde{y}(w) - \delta T(w)}{\delta} \\ \\ n_g(w(t)) \triangleq \sum_{i=1}^{N_T} n_{g_i}(w(t)) \triangleq \sum_{i=1}^{N_T} A_i^\pm(w(t)) \delta(w(t) - T_i). \\ \\ A_i^\pm(w(t)) \triangleq \begin{cases} 0 & w(t - \tau) = w(t) & \text{Glitch [3]} \\ A_i^- & w(t - \tau) > w(t) & \text{Nonlinearity} \\ A_i^+ & w(t - \tau) < w(t) \end{cases} \end{array} \right\} \text{Element mismatch Nonlinearity [8]}$$

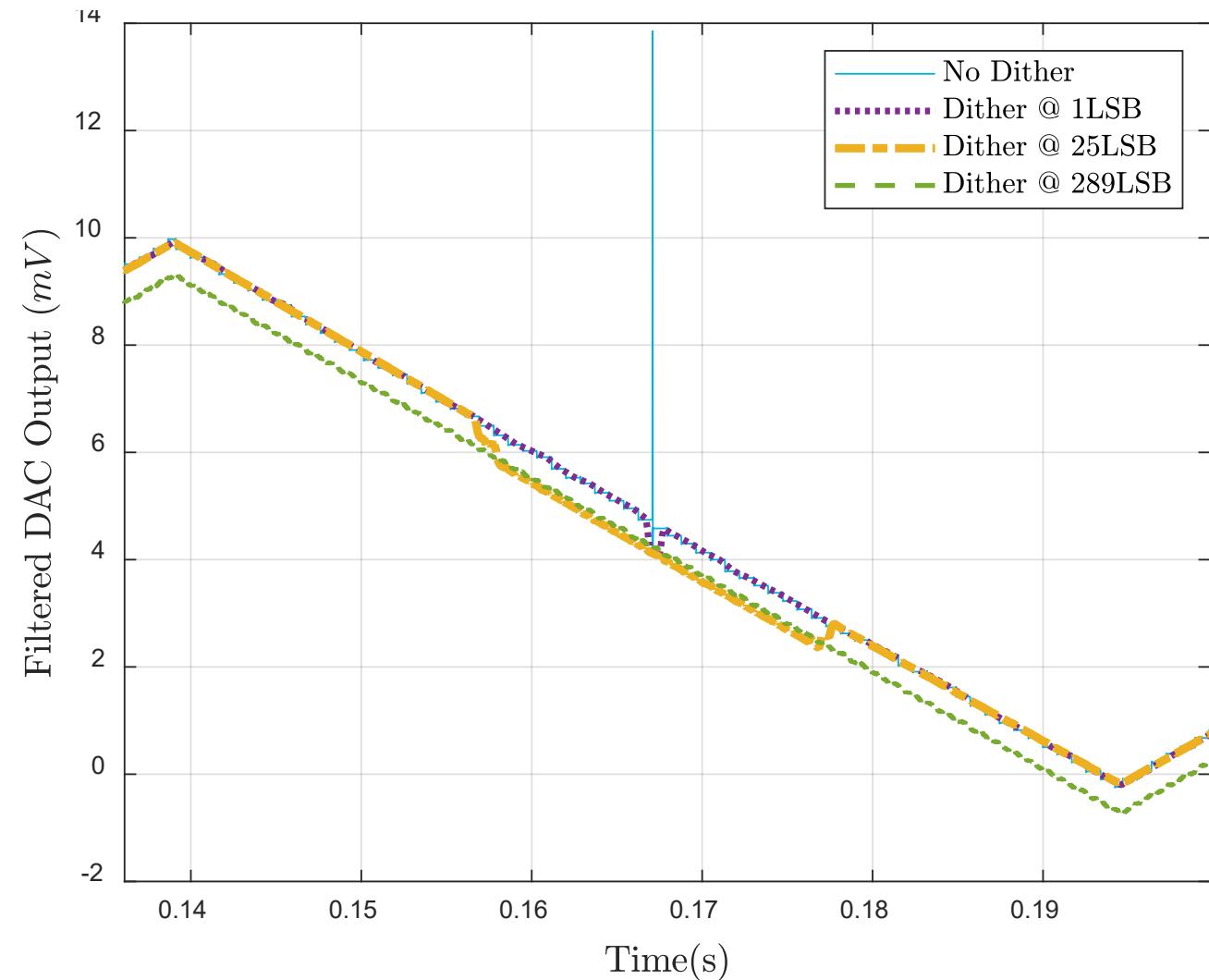


A GLITCH IN OPEN-LOOP

- Smoothed glitch due to periodic dither injection and filtering.

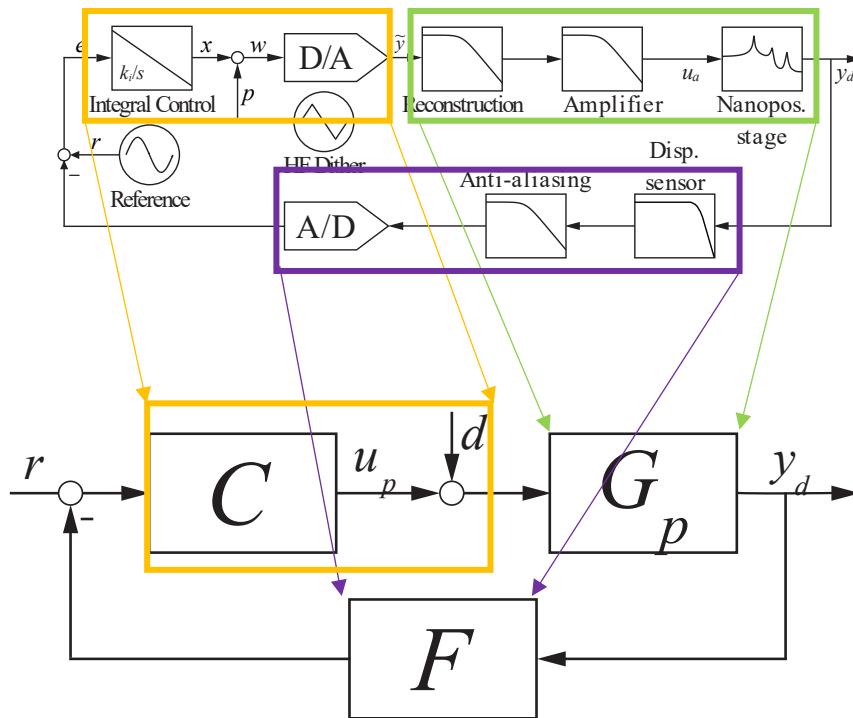


[9]



CONTROLLER DESIGN CHOICE EFFECT OVER DISTURBANCE REJECTION PERFORMANCE IN TANDEM WITH DITHER INJECTION

[5]



$$y_d = r \Rightarrow T(s) = 1$$

$$J(\theta_c) = \|1 - |T(j\omega; \theta_c)|\|_2$$

$$\theta_c = [\omega_c \ k_i]^T$$

$$\theta_c^* = \operatorname{argmin}_{\theta_c} J(\theta_c) : \operatorname{Re}\{\lambda_i\} \in \mathbb{R}_-$$

Nominal Design
(Nyquist Criterion)

$$C_i(s) = \frac{\omega_c^2}{s^2 + \sqrt{2}\omega_c s + \omega_c^2} \frac{k_i}{s}$$

Damping Integral
Incorporated Design

$$C_i(s) = \frac{k_i}{s}$$

Performance Measure $D(s)$:

$D(s)$ the transfer function from a disturbance d to the plant displacement y_d :

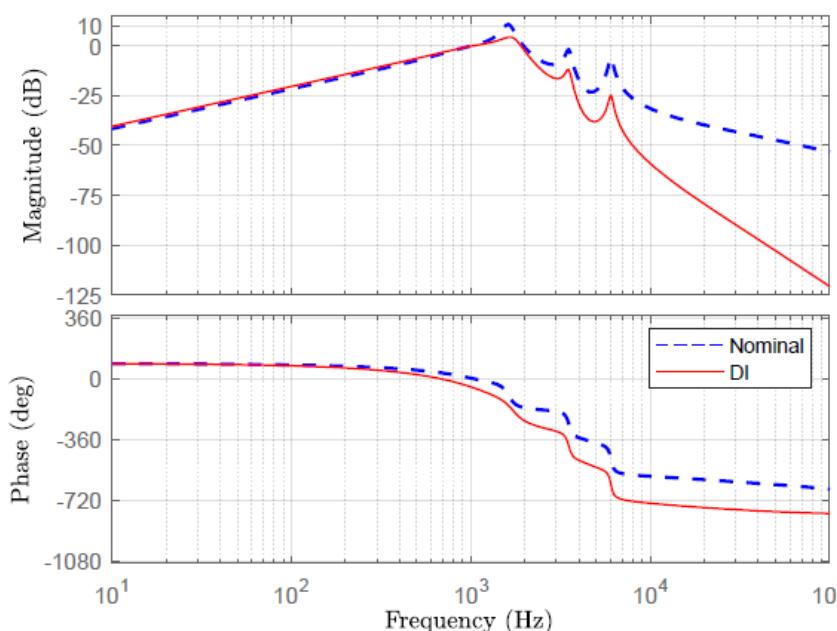
$$y_d = S(s)G_p(s)d = D(s)d$$

$S(s)$ the sensitivity of plant input u_p to a disturbance d :

$$u_p = (1 + L(s))^{-1}d = S(s)d$$

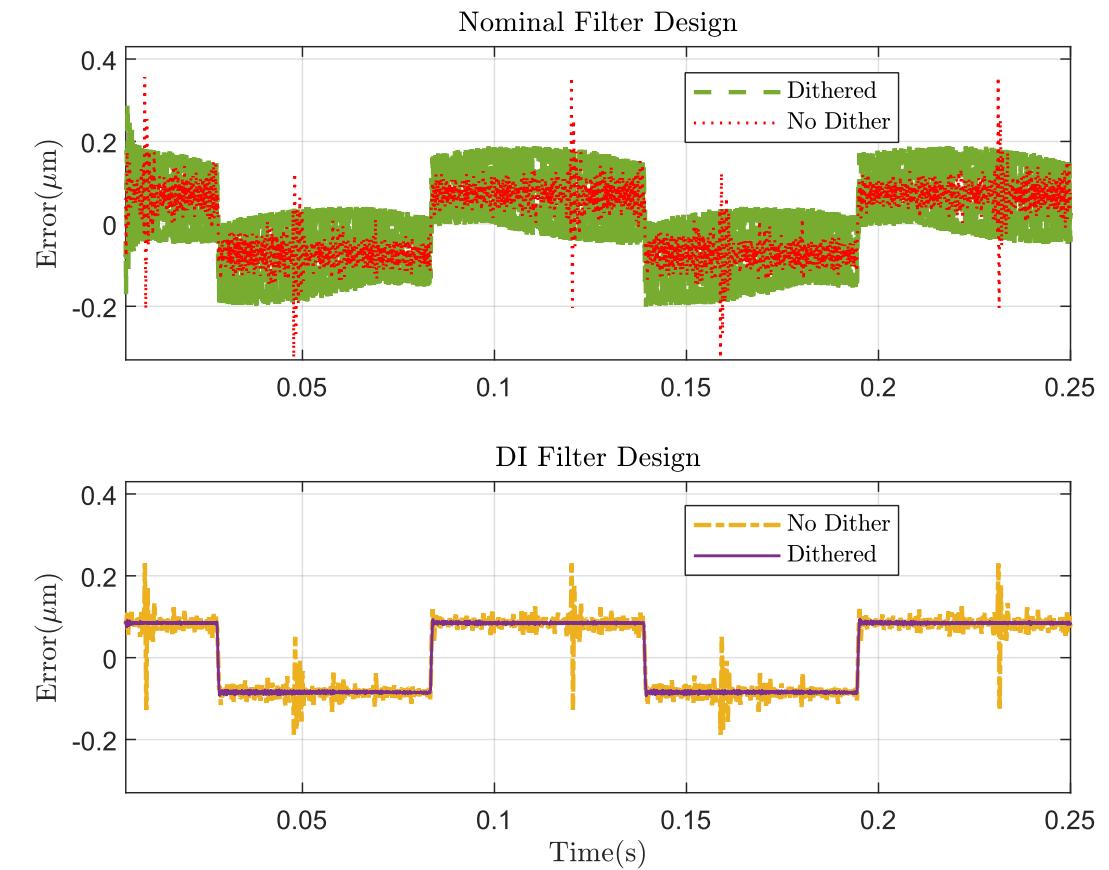
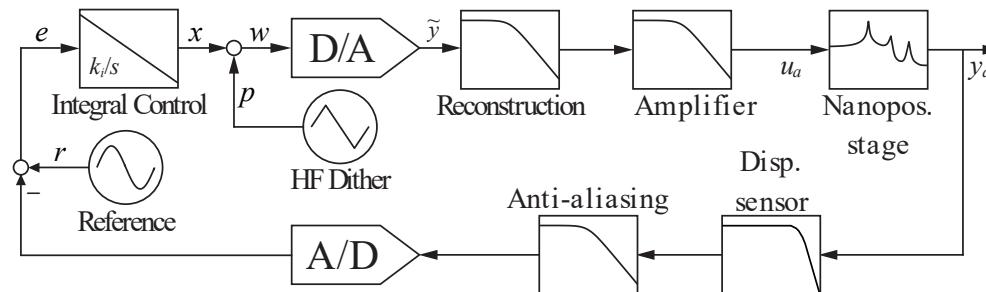
$L(s)$ loop transfer function, breaking the loop at u_p :

$$L(s) = C(s)F(s)G_p(s)$$



GLITCH DISTURBANCE IN CLOSED-LOOP

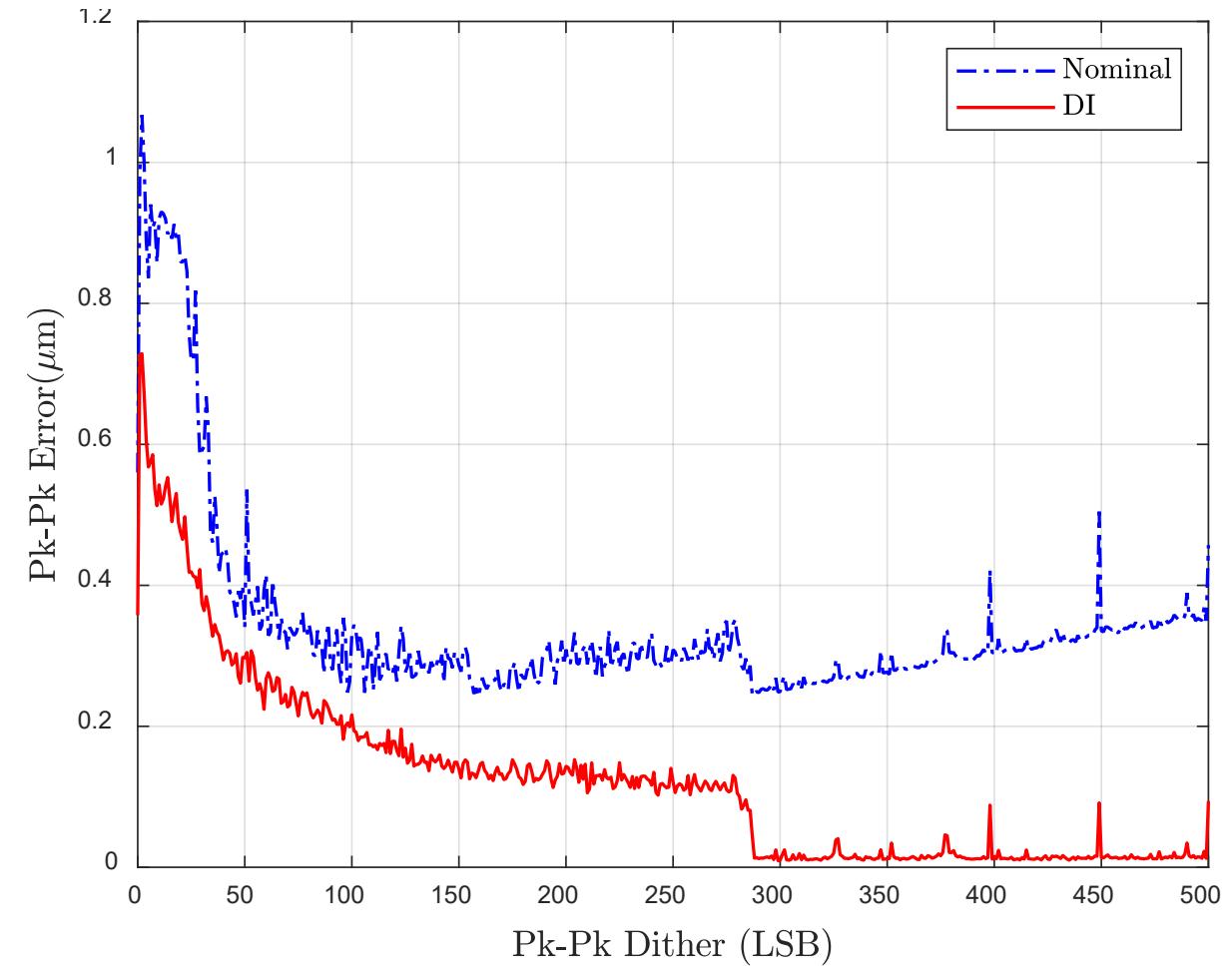
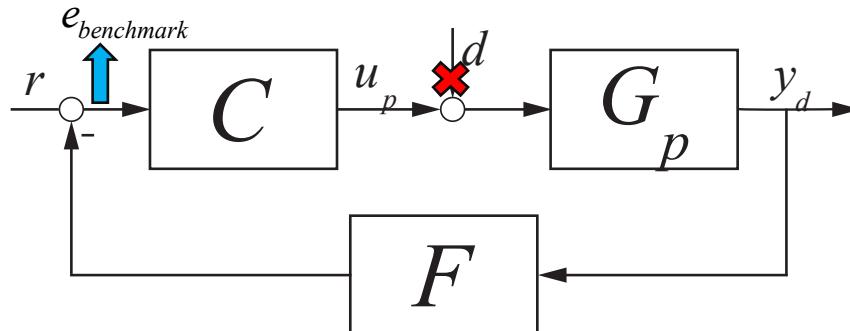
- Tracking error e due to a glitch disturbance smoothed by periodic dither injection and filtering.



GLITCH DISTURBANCE IN CLOSED-LOOP

- Residual tracking error e_r due to a glitch disturbance smoothed by periodic dither injection and filtering.

$$e_r = e - e_{benchmark}$$



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THANK YOU

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